



Technical description of the site plan, detailing lot dimensions, setbacks, and proposed structures.



Table with 2 columns: 'Lot No.' and 'Area (sq. ft.)'. It lists lot numbers and their corresponding areas.

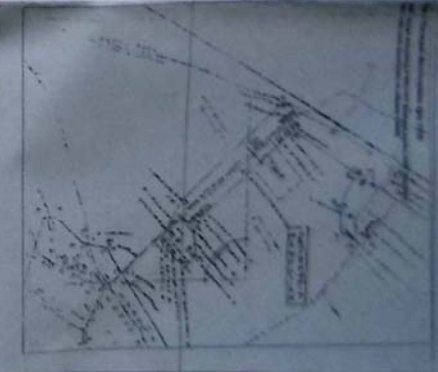
Professional engineer's signature and seal, along with project information and a date.



FIGURE A

Technical description of the aerial site plan, detailing the proposed building footprint and site boundaries.

Professional engineer's signature and seal, along with project information and a date.



Technical description of the aerial site plan, detailing the proposed building footprint and site boundaries.

Professional engineer's signature and seal, along with project information and a date.

Official stamps and signatures, including the professional engineer's seal and the title 'ANDREWS ENGINEER'.

ΠΙΝΑΚΑΣ Π-1 : ΑΡΧΙΚΟ ΓΗΠΕΔΟ

Με τη βοήθεια
των ορθογωνικών συντεταγμένων
των κορυφών του

| ΣΗΜΕΙΟ | X | Y | ΜΗΚΟΣ |
|--------|-----------|------------|-------|
| 1 | 297730.57 | 4228816.85 | |
| 2 | 297676.33 | 4228883.35 | 85.81 |
| 3 | 297679.31 | 4228886.02 | 4.00 |
| 4 | 297686.78 | 4228892.75 | 10.06 |
| 5 | 297690.56 | 4228896.18 | 5.11 |
| 6 | 297701.43 | 4228905.98 | 14.63 |
| 7 | 297703.29 | 4228907.82 | 2.61 |
| 8 | 297711.07 | 4228914.54 | 10.28 |
| 9 | 297720.82 | 4228923.60 | 13.31 |
| 10 | 297727.45 | 4228929.59 | 8.93 |
| 11 | 297736.61 | 4228937.68 | 12.22 |
| 12 | 297747.28 | 4228947.46 | 14.48 |
| 13 | 297751.21 | 4228951.06 | 5.33 |
| 14 | 297752.22 | 4228950.31 | 1.25 |
| 15 | 297767.76 | 4228940.22 | 18.53 |
| 16 | 297779.79 | 4228932.53 | 14.28 |
| 17 | 297793.99 | 4228923.21 | 16.98 |
| 18 | 297806.34 | 4228915.44 | 14.60 |
| 19 | 297813.56 | 4228910.62 | 8.68 |
| 20 | 297825.35 | 4228903.11 | 13.98 |
| 21 | 297832.44 | 4228898.93 | 8.23 |
| 22 | 297828.16 | 4228895.40 | 5.55 |
| 23 | 297818.37 | 4228887.33 | 12.69 |
| 24 | 297812.76 | 4228882.62 | 7.32 |
| 25 | 297808.31 | 4228879.19 | 5.62 |
| 26 | 297801.91 | 4228874.01 | 8.23 |
| 27 | 297800.54 | 4228872.99 | 1.70 |
| 28 | 297793.56 | 4228867.20 | 9.07 |
| 29 | 297788.25 | 4228862.77 | 6.92 |
| 30 | 297776.88 | 4228853.68 | 14.55 |
| 31 | 297775.43 | 4228852.65 | 1.77 |
| 32 | 297770.06 | 4228848.20 | 6.98 |
| 33 | 297764.45 | 4228843.55 | 7.28 |
| 34 | 297758.27 | 4228838.35 | 8.08 |
| 35 | 297755.02 | 4228835.95 | 4.04 |
| 36 | 297743.69 | 4228827.42 | 14.18 |
| 37 | 297732.75 | 4228818.63 | 14.04 |
| 38=1 | 297730.57 | 4228816.85 | 2.81 |
| 1 | 297730.57 | 4228816.85 | 0.00 |

$$E = 1/2 \sum (X_i + X_{i+1})(Y_i - Y_{i+1})$$

$$E = 10323.14 \mu^2$$

ΠΙΝΑΚΑΣ Π-10α : Τμήμα ΕΝΤΟΣ οικισμού

Με τη βοήθεια
των ορθογωνικών συντεταγμένων
των κορυφών του

| ΣΗΜΕΙΟ | X | Y | ΜΗΚΟΣ |
|----------|-----------|------------|-------|
| 1 | 298230.57 | 4228816.85 | 85.81 |
| 2 | 298176.33 | 4228883.35 | |
| 3 | 298179.31 | 4228886.02 | 4.00 |
| 4 | 298186.78 | 4228892.75 | 10.06 |
| 5 | 298190.57 | 4228896.19 | 5.12 |
| 6 | 298201.43 | 4228905.98 | 14.63 |
| 7 | 298203.29 | 4228907.82 | 2.61 |
| 8 | 298211.07 | 4228914.54 | 10.28 |
| 9 | 298220.82 | 4228923.60 | 13.31 |
| 10 | 298227.45 | 4228929.59 | 8.93 |
| 11 | 298236.61 | 4228937.68 | 12.22 |
| 12 | 298247.28 | 4228947.46 | 14.48 |
| 12' | 298249.90 | 4228949.85 | 3.54 |
| κορυφή 8 | 298220.26 | 4228908.61 | 50.79 |
| 32' | 298269.74 | 4228847.94 | 78.29 |
| 33 | 298264.45 | 4228843.55 | 6.87 |
| 34 | 298258.27 | 4228838.35 | 8.08 |
| 35 | 298255.02 | 4228835.95 | 4.04 |
| 36 | 298243.84 | 4228827.54 | 13.99 |
| 37 | 298232.75 | 4228818.63 | 14.23 |
| 1 | 298230.57 | 4228816.85 | 2.81 |

$$E = 1/2 \sum (X_i + X_{i+1})(Y_i - Y_{i+1})$$

$$E \text{ (εντός οικισμού)} = 4633.91 \mu^2$$

ΠΙΝΑΚΑΣ Π-10β : Τμήμα ΕΚΤΟΣ οικισμού

Με τη βοήθεια
των ορθογωνικών συντεταγμένων
των κορυφών του

| ΣΗΜΕΙΟ | X | Y | ΜΗΚΟΣ |
|----------|-----------|------------|-------|
| 13 | 298251.21 | 4228951.06 | |
| | | | 1.25 |
| 14 | 298252.22 | 4228950.31 | 18.53 |
| 15 | 298267.76 | 4228940.22 | 14.28 |
| 16 | 298279.79 | 4228932.53 | 16.98 |
| 17 | 298293.99 | 4228923.21 | 14.60 |
| 18 | 298306.34 | 4228915.44 | 8.68 |
| 19 | 298313.56 | 4228910.62 | 13.98 |
| 20 | 298325.35 | 4228903.11 | 8.23 |
| 21 | 298332.44 | 4228898.93 | 5.55 |
| 22 | 298328.16 | 4228895.40 | 12.69 |
| 23 | 298318.37 | 4228887.33 | 7.32 |
| 24 | 298312.76 | 4228882.62 | 5.62 |
| 25 | 298308.31 | 4228879.19 | 8.23 |
| 26 | 298301.91 | 4228874.01 | 1.70 |
| 27 | 298300.54 | 4228872.99 | 9.07 |
| 28 | 298293.56 | 4228867.20 | 6.92 |
| 29 | 298288.25 | 4228862.77 | 14.55 |
| 30 | 298276.88 | 4228853.68 | 1.77 |
| 31 | 298275.43 | 4228852.65 | 6.98 |
| 32 | 298270.06 | 4228848.20 | 0.41 |
| 32' | 298269.74 | 4228847.94 | 78.29 |
| κορυφή 8 | 298220.26 | 4228908.61 | 50.79 |
| 12' | 298249.90 | 4228949.85 | 1.79 |
| 13 | 298251.21 | 4228951.06 | |

$$E = 1/2 \sum (X_i + X_{i+1})(Y_i - Y_{i+1})$$

$$E \text{ (ΕΚΤΟΣ)} = 5689.23 \mu^2$$